

Nonlinear Model Predictive Control for Solid-Oxide Electrolysis Cell Systems

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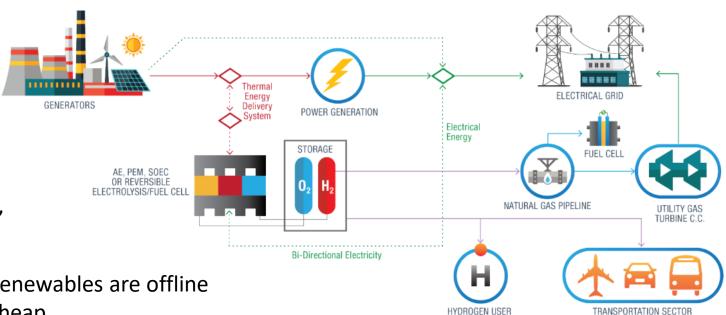
Tightly-coupled Integrated Energy Systems (IES) play an important role in load-balancing

 Intermittent renewable energy adds volatility to electricity prices

 IES can leverage capabilities of diverse energy generators to provide heat, power, mobility and storage



Produce hydrogen while electricity is cheap



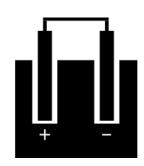
How fast can these systems switch between operating points?

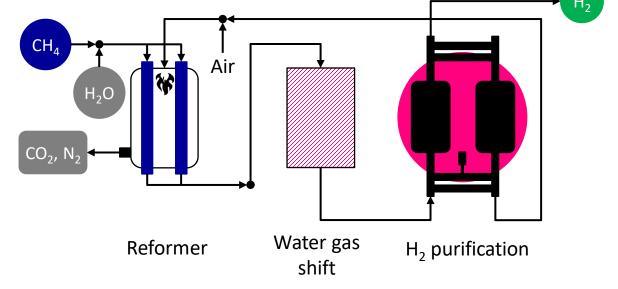


Hydrogen production will play a crucial role in the energy transition and decarbonization

 Most industrial hydrogen is produced through steam-methane reforming, which uses fossil fuels as feedstock

 Water electrolysis is a potential replacement, producing no direct greenhouse gas emissions when renewable energy is used

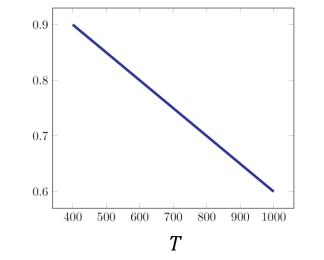




Nernst potential decreases with increasing reaction temperature

The minimum potential difference at which electrolysis can occur

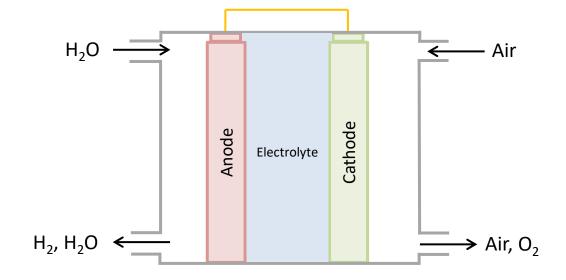
$$E_{\text{cell}} = E^0 - \frac{RT}{nF} \ln Q$$





Solid-oxide electrolysis cells (SOECs) are candidates for efficient electrolysis

- SOECs operate at 600 °C to 1000 °C, much higher temperatures than other electrolysis technologies
- High temperature operation comes with significant drawbacks
 - Additional heat exchange equipment
 - Good thermal insulation
 - Careful control during transition between operating points

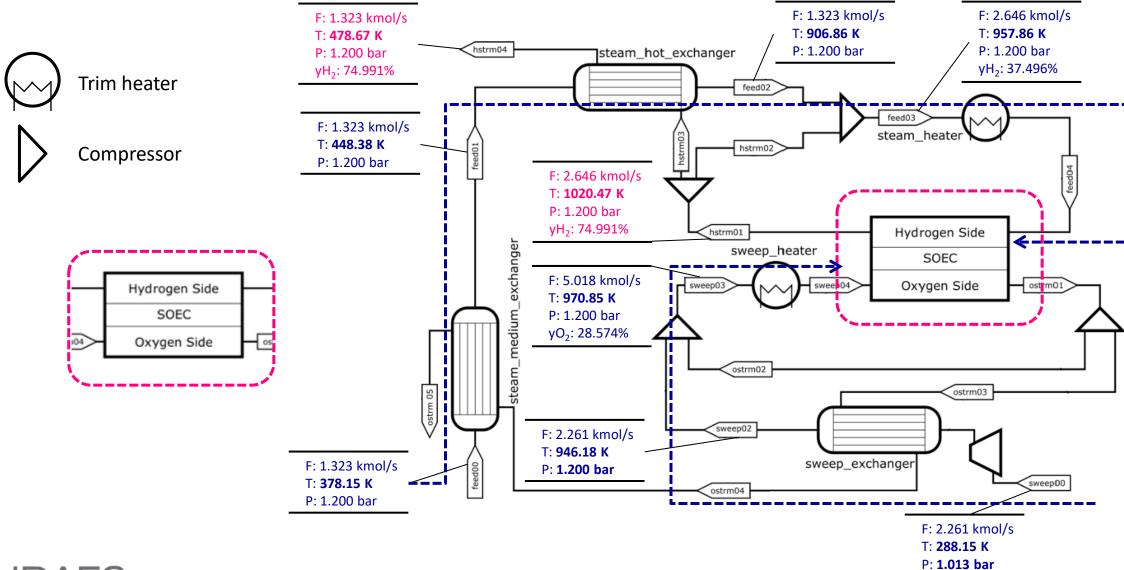


Electrolyte: hard, non-porous ceramic material

Dynamics, health modeling and **advanced process control** are needed to improve SOEC operational performance and thermal management while reducing cell degradation during frequent transients



Process flow diagram of SOEC flowsheet





Dynamic SOEC modeling as an integration of submodules

Anode (fuel) channel model

$$\frac{\partial C_{i,\text{ac}}}{\partial t} = -\frac{\partial}{\partial z} \left(C_{i,\text{ac}} u_{z,\text{ac}} \right) - \frac{J_{i,\text{ac}}}{x_{\text{in,an}}}$$

$$C_{i,\text{ac}} = C_{\text{total,ac}} y_{i,\text{ac}}$$

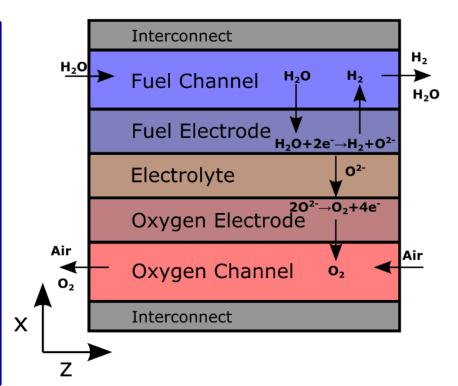
$$C_{\text{total,ac}} = f \left(P_{\text{ac}}, T_{\text{ac}}, y_{i,\text{ac}} \right)$$

$$\sum y_{i,\text{ac}} - 1 = 0$$

$$J_{i,\text{ac}} = -\mathcal{D}_{i,\text{eff}} \frac{\partial C_{i,\text{an}}}{\partial x} \mid_{x = x_{\text{in,an}}}$$

$$\mathcal{D}_{\text{H}_2}, \mathcal{D}_{\text{H}_2}\text{O}$$

C: molar density, J: flux, D: diffusivity, ac: anode channel, an: anode, i: species



Nonisothermal, planar SOEC

Fuel electrode: water is reduced into hydrogen

Oxygen electrode: electrode to which O²⁻ ions diffuse



Allan et al. (Under review)



Dynamic SOEC modeling as an integration of submodules

Anode (fuel electrode) model

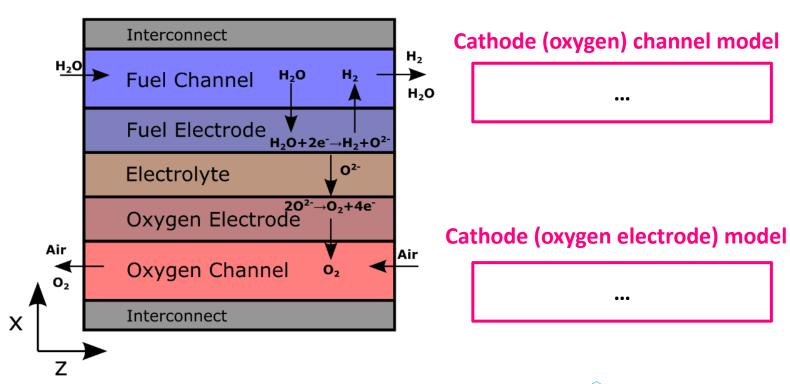
$$\varepsilon_{\rm an} \frac{\partial C_{i,\rm an}}{\partial t} = \frac{\partial^2}{\partial z^2} \left(\mathcal{D}_{i,\rm eff} C_{i,\rm an} \right)$$

$$C_{i,\mathrm{an}} = C_{\mathrm{total,an}} y_{i,\mathrm{an}}$$

$$C_{\text{total,an}} = f(P_{\text{an}}, T_{\text{an}}, y_{i,\text{an}})$$

$$\sum y_{i,\mathrm{ac}} - 1 = 0$$

C: concentration, J: flux, D: diffusivity, ac: anode channel, an: anode, i: species



Electrochemical model

- Activation polarization at the cathode and anode
- Ohmic polarization



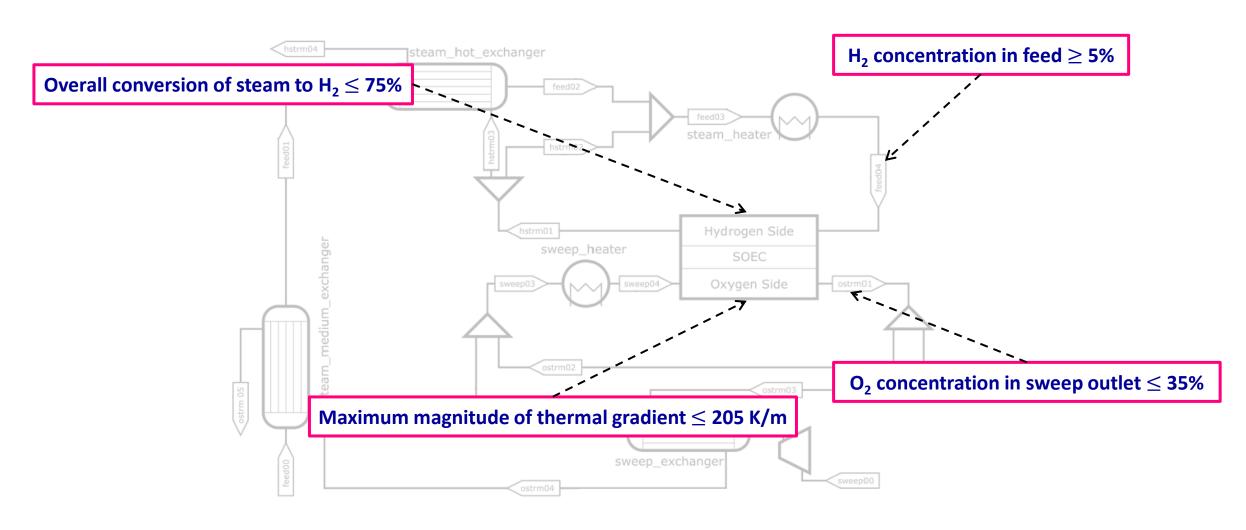
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Allan et al. (Under review)

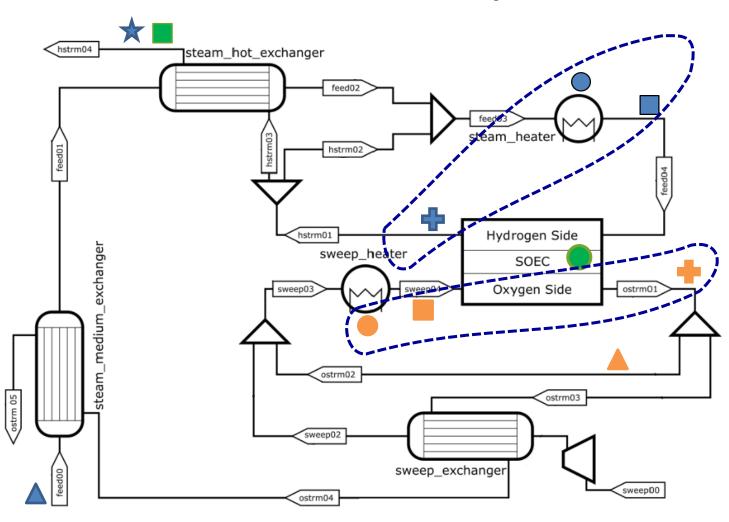


System performance constraints





Classical process control pairings







Nonlinear Model Predictive Control (NMPC) can handle highly interactive manipulated variables

NMPC framework developed for setpoint transition using the same 7 manipulated variables

$$f_{\text{obj}} = \sum_{i=0}^{N} \rho_{\text{H}_2} \left(y_i - y_i^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \rho_j \left(u_{ij} - u_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{k \in K} \rho_k' \left(x_{ik} - x_{ik}^R \right)^2 + \sum_{i=1}^{N} \rho' \left(\nu_i - \nu_{i-1} \right)^2 + \rho_s \sum_{i=0}^{N} \sum_{z=1}^{Z_L} \left(p_{iz} + n_{iz} \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij} - y_{ij}^R \right)^2 + \sum_{i=0}^{N} \sum_{j \in J} \left(p_{ij}$$

Trajectory tracking of H₂ production rate Deviations of manipulated (u_{ij}) and controlled variables (x_{ik}) from reference values

Rate of change penalties on trim heater duties

 ℓ_{1} -penalties for temperature gradient constraints

To prevent thermal degradation over time, the magnitude of the temperature gradient along the cell length (z-direction) is constrained to be below 205 K/m

$$\frac{dT}{dz} - 205 \le p$$
 and $-\frac{dT}{dz} - 205 \le n$

An ℓ_1 -penalty relaxation treats them as soft constraints with non-negative slack variables p and n penalized in the objective



Dynamic simulation and control solution approaches to compare classical control with NMPC

Case study: ramp H₂ production

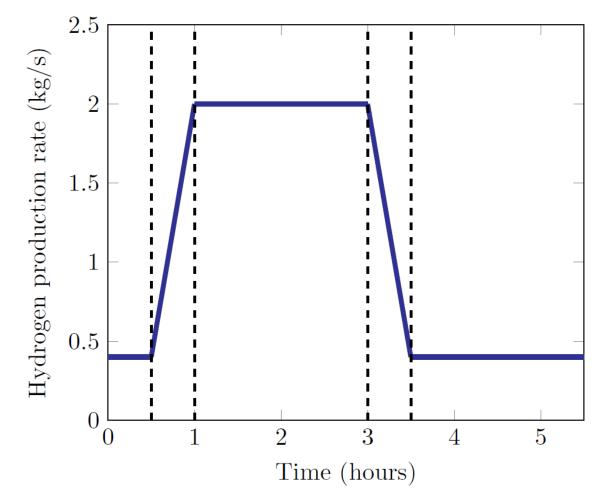
- Minimum (0.4 kg/s) to maximum (2.0 kg/s) and back to minimum
- Each ramp performed over 30 min followed by 2 hrs of settling time

Solution approach

- Classical: PETSc variable step implicit Euler DAE solver
- NMPC: Full-discretization NLP with IPOPT solver

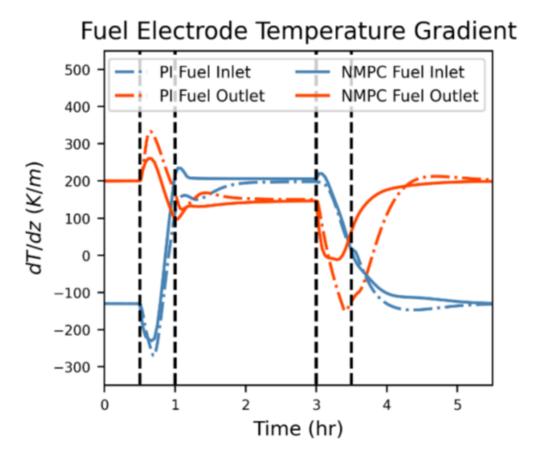
Problem size

- Approximately 16000 equations and variables
- Average solution time of 35.5s for a prediction horizon of 750s

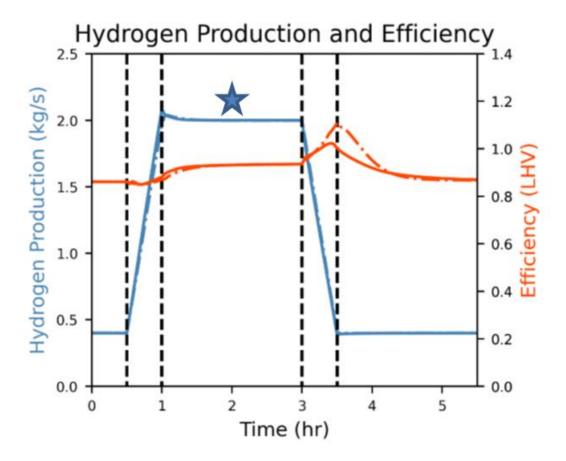




Dynamic simulation and control results



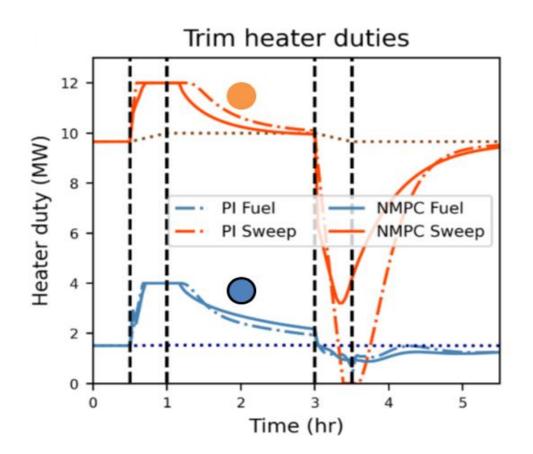
NMPC contains thermal gradients significantly better than sophisticated classical control

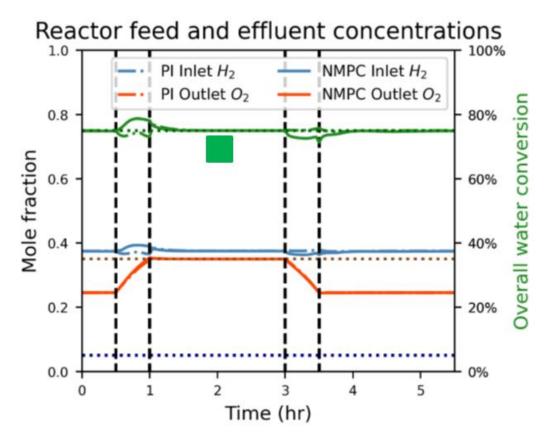


- Hydrogen production tracking is identical
- Efficiency for NMPC is lower during transients as it is takes into account the restriction of thermal degradation



Dynamic simulation and control results



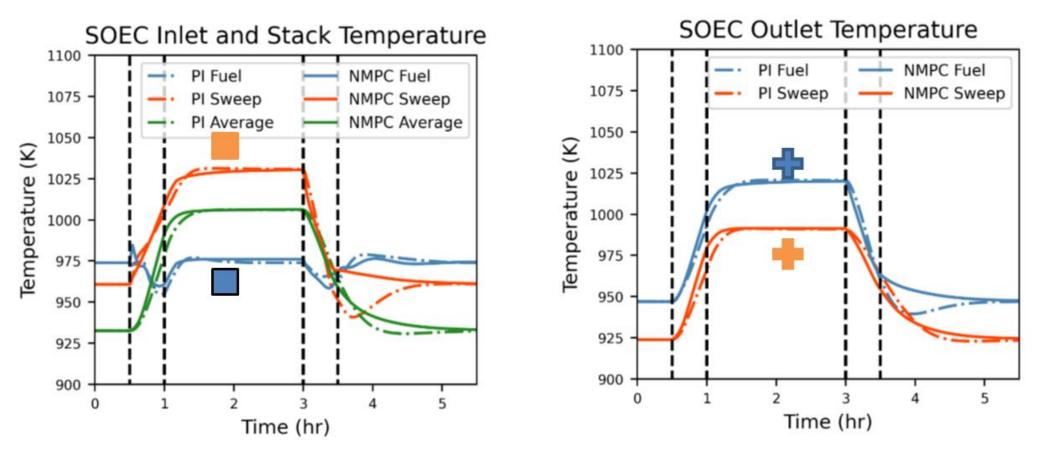


Settling of trim heater duties is faster with NMPC

Performance constraints are satisfied, slight violations during transients



Dynamic simulation and control results



NMPC yields a quicker response in terms of settling of SOEC inlet, outlet and stack temperatures

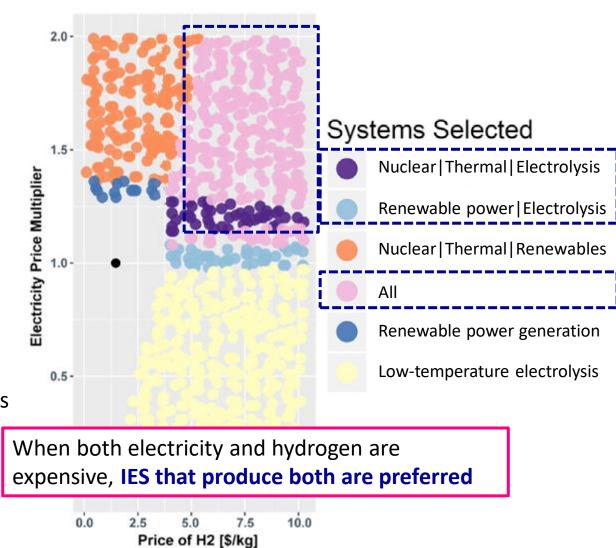


Conclusions, impacts and future directions

- IDAES offers an ecosystem of large-scale dynamic models for integrated energy systems, as well as classical and advanced control capabilities
- Setpoint tracking NMPC can restrict temperature gradients more effectively compared to classical control
- Matching the tracking performance of NMPC requires a sophisticated approach with cascade control – NMPC is suited to handle complex multiinput multi-output systems

Future work

- **Economic NMPC** with more general objective functions
- Effective mode switching between hydrogen production and power generation modes





idaes.org

github.com/IDAES/idaes-pse



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